

Parametric study of the performance of two-dimensional scramjet intake

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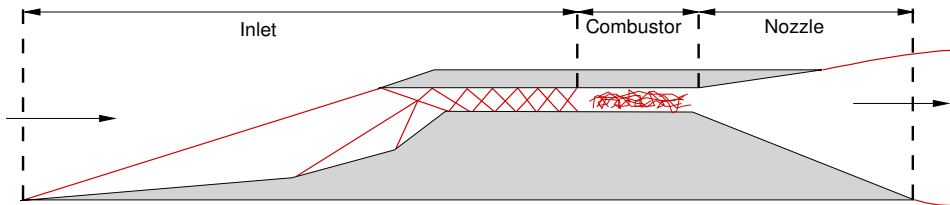


Outline

- 1 Schematic of scramjet engine
- 2 Objective
- 3 Inlet design
- 4 On-design condition
- 5 Mach effect
- 6 Effect of angle of attack
- 7 Effect of cowl deflection angle
- 8 Starting of intake
- 9 Summary



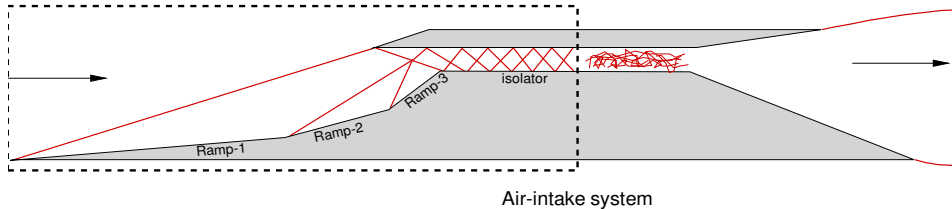
Schematic of scramjet engine



Schematic of scramjet engine



Primary objectives in designing efficient inlet



- ① Near to isentropic and high pressure recovery.
- ② High capture area (high mass flow).
- ③ Uniform flow.
- ④ Wide range of operation.



Performance parameters

Static temperature ratio

$$\psi = \frac{T_{exit}}{T_{inlet}}$$



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$$\pi_c = \frac{P_{o,exit}}{P_{o,inlet}}$$



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Kinetic energy efficiency

$$\eta_{KE} = 1 - 0.2 \left(1 - \frac{M_{exit}}{M_{inlet}} \right)^5$$



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Captured mass flow rate

$$\dot{m}_c = \rho A_c V_{inlet}$$



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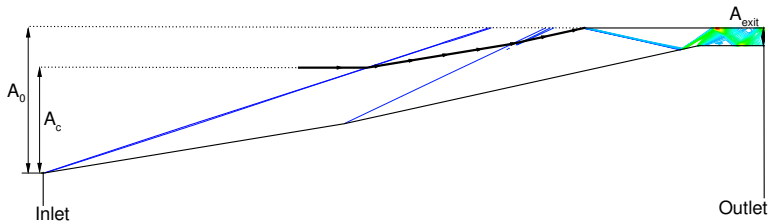
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Objective

- 1 Design a scramjet inlet (at a cruising flight Mach number-6.5).
- 2 Effect of angle of attack, α .
- 3 Effect of cowl deflection angle, θ_c .



Outline

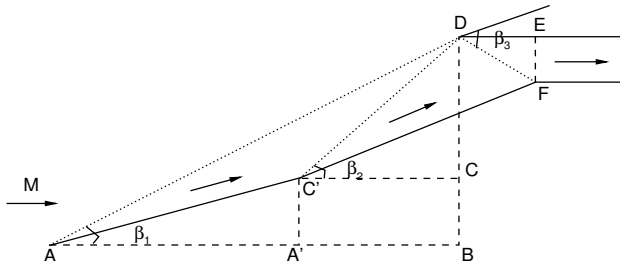
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Inlet Design

Design criteria:

- 1 Shock-on-lip condition
- 2 Uniform flow



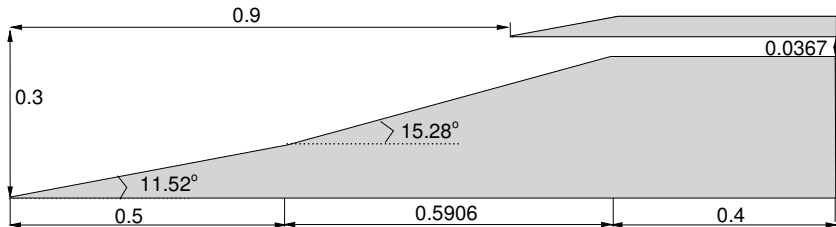
Input parameters

- 1 Mach number (M)
- 2 First ramp length (AA').
- 3 Distance of the cowl tip from the first ramp leading edge (AB).
- 4 Total intake height (DB).



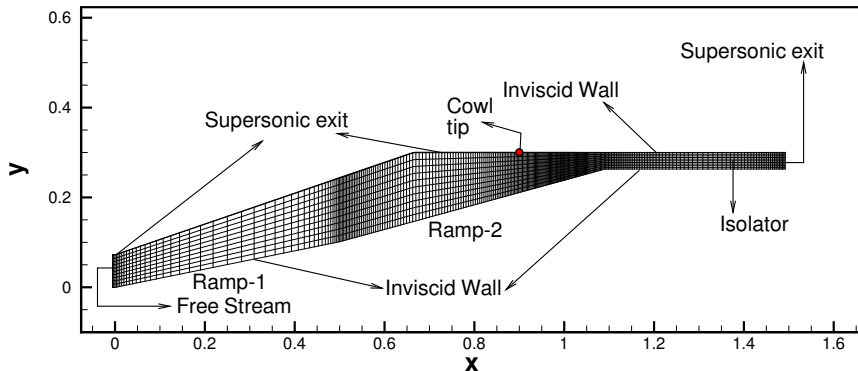
Physical and Computational domain

Details of scramjet intake geometry (All dimensions are in meters)



Physical and Computational domain

Grid structure and boundary conditions.



550 x 250 grid points, with x-stretching factor of 1.28



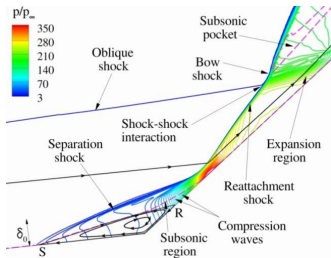
Numerical methodology

- ❶ In-house code
- ❷ Finite volume formulation
- ❸ Modified Steger-Warming flux splitting (*Computers and Fluids*, 1989)
- ❹ Implicit Data Parallel Line Relaxation method (*AIAA*, 1998)

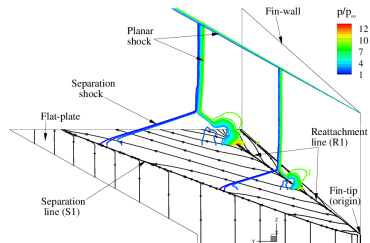


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J. Propul. Power (2012)



AeSI CFD Sym. (2009)

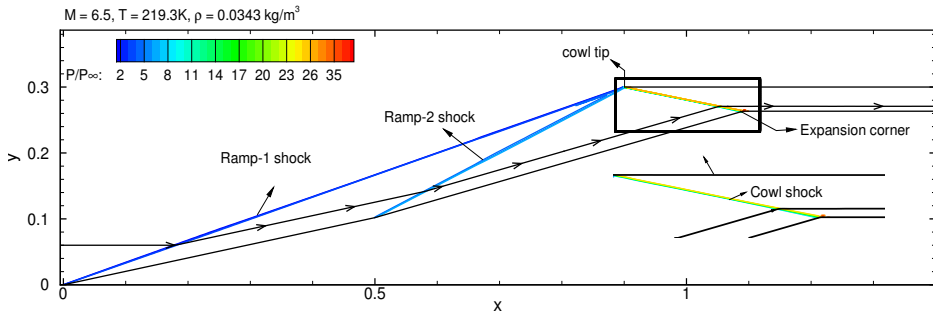


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On-design condition ($M = 6.5$)



Pressure contour of inlet for on-design Mach number at $\alpha = 0^\circ$ and $\theta_c = 0^\circ$.



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Mach effect

Table : Comparison of the analytical and numerical simulation results with respect to various parameters for scramjet inlet.

Mach	T_{iso}/T_{inlet}		$P_{o,iso}/P_{o,inlet}$		P_{iso}/P_{inlet}		M_{iso}	
	Theo.	CFD	Theo.	CFD	Theo.	CFD	Theo.	CFD
4.5	2.298	2.295	0.742	0.745	13.660	13.652	2.446	2.450
5.5	2.716	2.707	0.630	0.637	20.804	20.797	2.824	2.830
6.5	3.197	3.197	0.521	0.523	30.422	30.533	3.127	3.120
7.5	3.743	3.76	0.422	0.414	42.827	42.769	3.370	3.370

The difference is within the $\pm 2\%$ error range for all parameters.

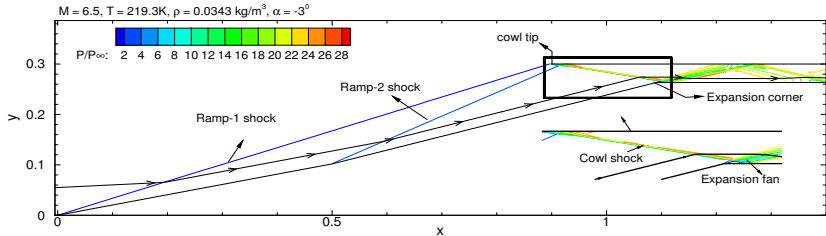
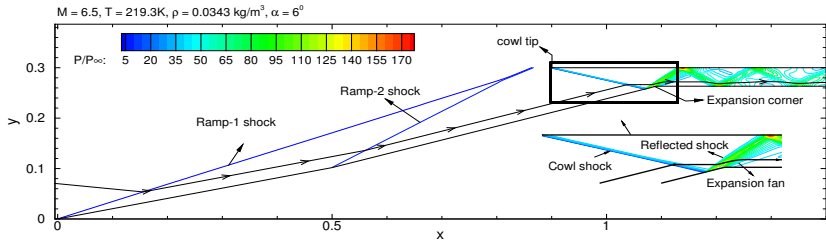


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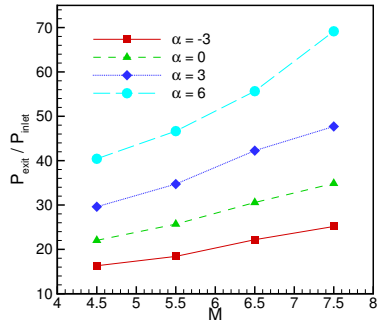
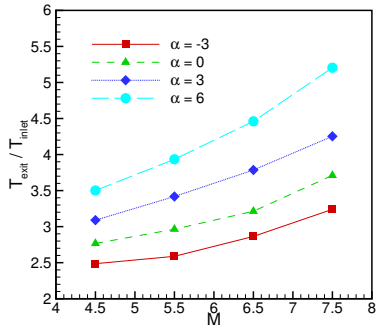
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Flow structure for varying α at $M = 6.5$

(a) $\alpha = -3^\circ$ (b) $\alpha = 6^\circ$

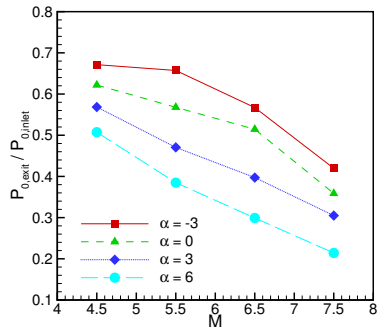
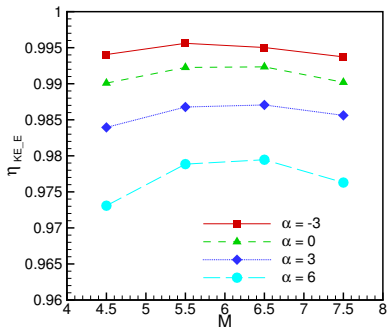
Performance parameters (varying α and M)



At the fixed angle of attack, the strength of the shocks increases with increasing Mach number



Continue...



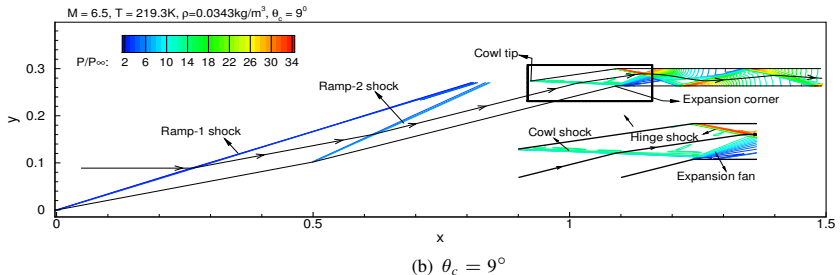
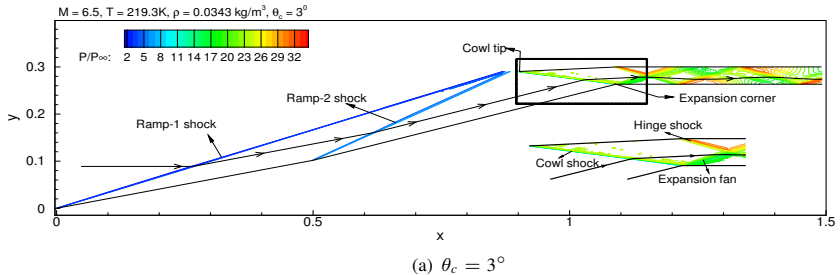
Maximum η_{KE} is observed at designed Mach number



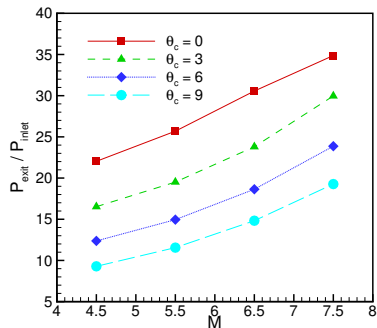
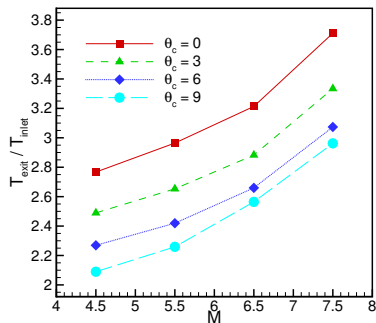
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Flow structure for varying θ_c at $M = 6.5$ 

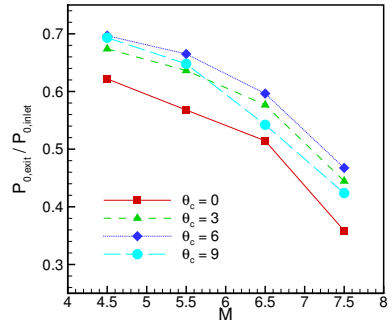
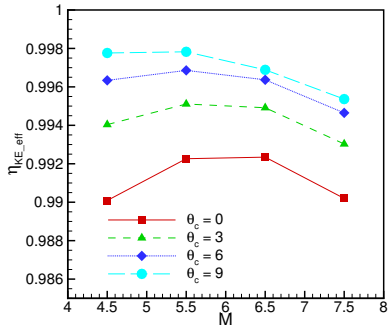
Performance parameters (varying Mach number and θ_c)



Compression ratios increases with M
Decreases with increasing θ_c



Continue...



$\uparrow \theta_c$ – shifts the maximum η_{KE} to lower Mach numbers



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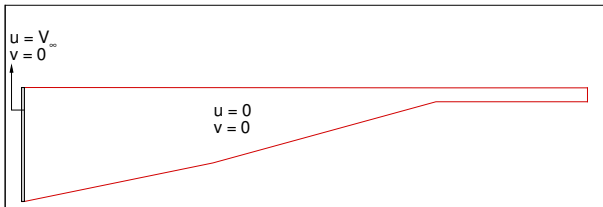
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Flow initialization



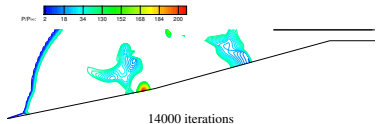
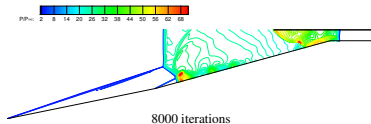
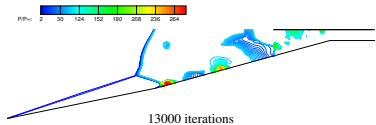
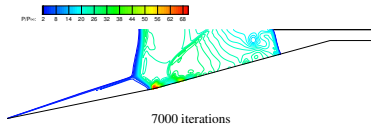
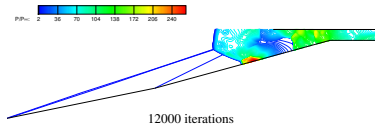
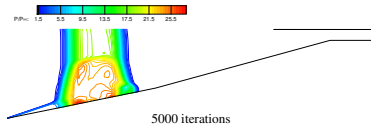
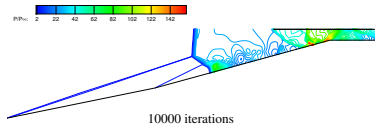
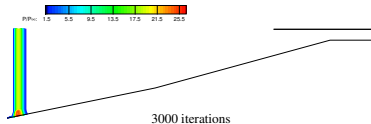
Earlier simulations: Free-stream velocity initialization



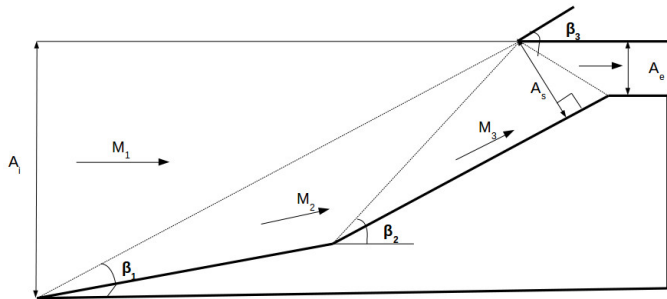
New Simulations: Zero velocity initialization



Unstarted mode



Starting criteria

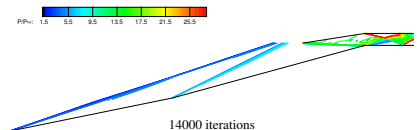
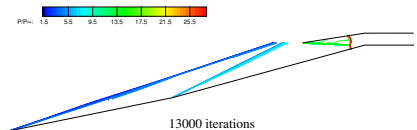
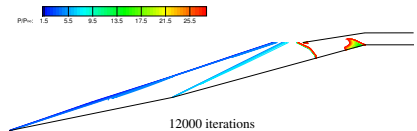
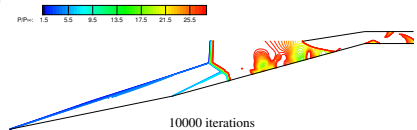
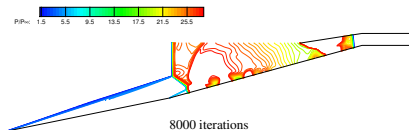
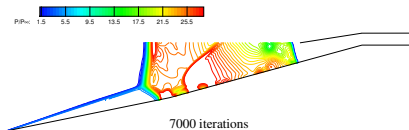
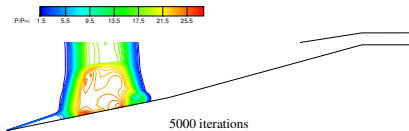
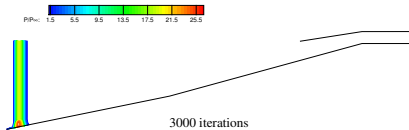


$$(A_e/A_s) \geq \left[\frac{\gamma - 1}{\gamma + 1} + \frac{2}{(\gamma + 1)M_3^2} \right]^{\frac{1}{2}} \left[\frac{2\gamma}{\gamma + 1} - \frac{\gamma - 1}{(\gamma + 1)M_3^2} \right]^{\frac{1}{\gamma - 1}}$$

A_e is fixed and reducing the A_s by deflecting the cowl to meet Kantrowitz criteria
Self starting is achieved , $\theta_c = 9^\circ$



Started mode



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Summary

- ❶ Performed inviscid numerical simulations of a typical mixed-compression scramjet intake.
- ❷ Studied its performance for a range of Mach numbers, angles of attack and cowl deflection angles.
- ❸ At off-design conditions, a set of shock and expansion fans are generated in the intake duct, and they reflect between the duct walls.
- ❹ It is found that the maximum pressure recovery is obtained at lower Mach number with weaker shock waves, and the capture mass flow rate is maximum at higher Mach numbers.
- ❺ As the cowl angle is increased, the maximum kinetic energy efficiency is obtained at Mach numbers lower than the design point.
- ❻ At zero velocity initialization, intake starts with deflection of cowl.



Thank you...